Influence of Wall Construction on the Acoustical Behaviour of ETHICS

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1 Introduction

External thermal insulation composite systems (ETHICS) are used to improve the heat insulation of the outer walls of buildings. In addition they change the acoustical properties of the walls. Depending on construction (thickness and stiffness of the insulating layer, mass of the plaster coat) the sound insulation can be either increased or reduced [1].

According to the basic acoustical model, which is based on a simple mass-spring-mass system, the improvement of sound insulation by ETHICS doesn't depend on the kind of the supporting wall. In practice, however, this simplification only applies to heavy, massive walls. For light walls consisting of perforated bricks or bricks with low density the interaction between wall and ETHICS can't be neglected. Systematic investigations of the acoustical interaction are so far missing. In the article in hand we present some examples to illustrate the relation between wall construction and the improvement of sound insulation by ETHICS.

2 Construction of ETHICS

ETHICS consist of heat insulating plates (mostly rigid foam polystyrene or mineral fibre), which are fixed onto the outer surface of the wall and covered by a plaster coat. The fixation is performed by adhesive mortar and sometimes additionally by dowels. The thickness of the insulating layer typically ranges from about 80 to 200 mm. An example for the construction of ETHICS is shown in the following picture:

![Fig. 1 Construction of ETHICS.](image)

3 Theory

In principle ETHICS can be represented by two rigid masses (plaster coat and wall) which are connected by a spring (insulating layer). Since the mass of the plaster coat is generally much smaller than that of the wall, the frequency of the double leaf resonance fr is given by

\[ f_r = \left(\frac{1}{2\pi}\right)\sqrt{s'/m''}, \quad (1) \]

with \( s' = \frac{E}{d} \) = dynamic stiffness of the insulating layer, \( E \) = dynamic modulus of elasticity, \( d \) = thickness of the insulating layer, 
\( m'' \) = mass per unit area of the supporting wall.

In practice the dynamic stiffness of the insulating layer takes values of about 2 MN/m² ≤ \( s' \) ≤ 50 MN/m² resulting in a resonance frequency in the range of 50 Hz ≤ \( f_r \) ≤ 500 Hz [2]. Depending on \( f \) the frequency response of the transmission loss contains three characteristic regions:

- For \( f << f_r \) the transmission loss of the supporting wall remains almost unchanged. The acoustical effect of ETHICS is negligibly small.
- In the range of the resonance frequency \( f \approx f_r \) a reduction of transmission loss occurs. The strength of the reduction depends on the damping of the system.
- For \( f >> f_r \) the sound insulation of the supporting wall is improved. The transmission loss increases by 18 dB per octave band compared to 6 dB per octave band without ETHICS.

4 Improvement of sound insulation

The improvement of the sound insulation by ETHICS is defined as

\[ \Delta R = R_E - R_s . \quad (2) \]

with \( R_E \) = transmission loss of the wall with ETHICS, \( R_s \) = transmission loss of the wall without ETHICS.

The weighted improvement \( \Delta R_w \) is determined by analogy as difference of the weighted sound reduction indices with and without ETHICS:

\[ \Delta R_w = R_{E,w} - R_{s,w} . \quad (3) \]

On condition that \( \Delta R \) is independent of the construction of the supporting wall the transmission loss of any wall can in principle be determined by

\[ R = R_s + \Delta R . \quad (4) \]

In practice, however, the validity of Eq. (4) is restricted, because \( \Delta R \) in some cases considerably depends on wall construction.

5 Investigated systems

Since systematic investigations were missing we searched for measurements which could provide information on the interaction between ETHICS and supporting wall. From our collection of data we chose two pairs of measurements, where identical ETHICS were combined with different walls. The construction of the systems is described in the following table:

<table>
<thead>
<tr>
<th>No.</th>
<th>Supporting Wall</th>
<th>ETHICS</th>
<th>d [mm]</th>
<th>m'' [kg/m²]</th>
<th>Insulation</th>
<th>d [mm]</th>
<th>m'' [kg/m²]</th>
</tr>
</thead>
<tbody>
<tr>
<td>1a</td>
<td>slb</td>
<td>eps</td>
<td>115</td>
<td>215</td>
<td>200</td>
<td>32</td>
<td></td>
</tr>
<tr>
<td>1b</td>
<td>slb</td>
<td>eps</td>
<td>240</td>
<td>460</td>
<td>200</td>
<td>31</td>
<td></td>
</tr>
<tr>
<td>2a</td>
<td>slb</td>
<td>mf</td>
<td>175</td>
<td>360</td>
<td>80</td>
<td>8</td>
<td></td>
</tr>
<tr>
<td>2b</td>
<td>vcb</td>
<td>mf</td>
<td>300</td>
<td>240</td>
<td>80</td>
<td>8</td>
<td></td>
</tr>
</tbody>
</table>

| d     | thickness of supporting wall or insulating layer |
| m''   | mass per unit area of supporting wall or outer plaster coat |
| slb   | solid lime-sand brick |
| vcb   | vertical coring brick |
| eps   | extruded polystyrene |
| mf    | mineral fibre |

Tab. 1 Construction of the investigated walls.
The main acoustical properties of the walls are specified in Tab. 2:

<table>
<thead>
<tr>
<th>No.</th>
<th>$f_c$ [Hz]</th>
<th>$f_r$ [Hz]</th>
<th>$R_{w,w}$ [dB]</th>
<th>$\Delta R_w$ [dB]</th>
</tr>
</thead>
<tbody>
<tr>
<td>1a</td>
<td>255</td>
<td>80</td>
<td>46</td>
<td>19</td>
</tr>
<tr>
<td>1b</td>
<td>125</td>
<td>80</td>
<td>55</td>
<td>13</td>
</tr>
<tr>
<td>2a</td>
<td>175</td>
<td>125</td>
<td>52</td>
<td>0</td>
</tr>
<tr>
<td>2b</td>
<td>105</td>
<td>125</td>
<td>43</td>
<td>14</td>
</tr>
</tbody>
</table>

- $f_c$: critical frequency of supporting wall (calculated)
- $f_r$: double leaf resonance frequency
- $R_{w,w}$: weighted sound reduction index of supporting wall without ETHICS
- $\Delta R_w$: improvement of $R_w$ by ETHICS

**Tab. 2** Acoustical properties of the investigated walls. The results for $f_c$ are only approximations since they are based on estimated values of the elastic modulus.

### 6 Results

A typical example for the transmission loss with and without ETHICS is shown in Fig. 2:

![Fig. 2](image1.png)

Transmission loss $R$ [dB] vs. frequency [Hz] for wall 1a (see Tab. 2) with and without ETHICS.

According to the results in Tab. 2 the improvement of sound reduction by ETHICS can vary strongly if the supporting wall is changed. Examples for the dependence of the improvement on the construction of the supporting wall are shown in Fig. 3 and 4.

- The improvement of sound insulation depends on the relation between the critical frequency $f_c$ and the double leaf resonance frequency $f_r$. For $f < f_c$, the influence of the wall construction is only weak (see Fig. 3, $f < 315$ Hz). Otherwise there are strong differences already at low frequencies (see Fig. 4).
- The differences at high frequencies cannot be explained by $f_c$ and $f_r$. There must be further effects which influence the acoustical properties of ETHICS.
- For light walls with low transmission loss the improvement of sound insulation seems to be stronger.

### 7 Summary

According to the presented examples the improvement of sound insulation by ETHICS can strongly depend on the construction of the supporting wall. Since so far are not enough data available, additional investigations are required to enable a detailed explanation of this effect. Till then the transfer of the improvement to different walls have to be performed very carefully.

### 8 Literature